

# Antennas for Wireless Terminals

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**SUMMARY** This paper reviews antenna technologies for cellular phone terminal in Japan. In regard to the technologies two technical subjects are addressed: a diversity system and miniaturization of terminal size. These subjects provide motivation for studies on design methods for diversity antennas, development of built-in antennas, and control methods for surface current on terminal cavity. These studies are progressing.

**key words:** *antenna, wireless terminal, built-in, diversity,*

## 1. Introduction

Antenna technologies for cellular phone terminals have developed dramatically in line with the policy of NTT DoCoMo Inc., was the first service provider of a mobile communication system in Japan. NTT DoCoMo decided to employ a diversity receiving system for cellular phone terminals and tried to shrink the volumes of terminals. In view of these decisions, antenna researchers tackled various technical subjects, with the objective of mounting two antennas on a small area, namely the surface of a terminal. Three key technologies concerning the above-mentioned subjects were released in 1982.

Fujimoto and Hirasawa did the first important research [1], [2]. They investigated the influence of surface current on terminal cavity quantitatively; the results showed that the current produced an unexpected radiation. This influence had both an advantage and a disadvantage, that is, whereas the antenna bandwidth is improved, the radiation pattern is changed. Therefore other researchers subsequently studied this influence from various perspectives.

The second concerned development of planar inverted F antenna (PIFA) [3], [4]. Haruki and Kobayashi tried to construct slot antenna by using planar element on terminal cavity, and found that the antenna operates as inverted F antenna, which is a low-profile monopole antenna. The development of planar inverted F antenna influenced many researchers engaged in the study of built-in antennas, and this also emerged as an important technical subject.

The third major study was that of by Sawaya et al. [5]. They proposed a novel design method for diversity antenna for automobiles. This method employed antenna coupling to minimize correlation coefficient value between antennas. The method formed the basis of a design method for diversity antenna for wireless terminals. Since antenna coupling resulted in both improvements and degradations respecting diversity antenna performance, the design method for diversity antenna remained a research subject.

Tsunekawa and Taga started a comprehensive study of the above-mentioned three subjects, and it resulted in antennas of practical terminals [6]; such as the personal digital cellular system (PDC) and the personal handy phone system (PHS). These subjects continue to be addressed by many researchers.

This paper reviews research on terminal antennas in Japan.

Fujimoto released a review of antenna systems for mobile communications in Japan. The review included not only antenna technologies but also peripheral technologies of antennas; such as a propagation technologies and system technologies [7]. Tokumaru released a review of technologies for small antenna in Japan [8]. He reviewed antenna technologies in terms of theoretical approaches.

Therefore, this paper focuses on the main features of technical subjects concerning practical terminal antennas; namely, studies of current on terminal cavity, development of built-in antenna, and a design method for diversity antenna (Table 1). Furthermore, in order to introduce various technologies developed in Japan, this paper reviews papers and abstracts published in Japanese.

## 2. Study on a Current of a Terminal Cavity

NTT DoCoMo started cellular-phone service in Japan in 1986. The antenna used for the first cellular phone terminal was half-wavelength monopole antenna. Fujimoto and Hirasawa clarified that this antenna reduces current on cavity, in comparison with quarter-wavelength monopole antenna [1], [2].

### 2.1 Influence of Current on Cavity

Fujimoto and Hirasawa, who have focused on the influ-

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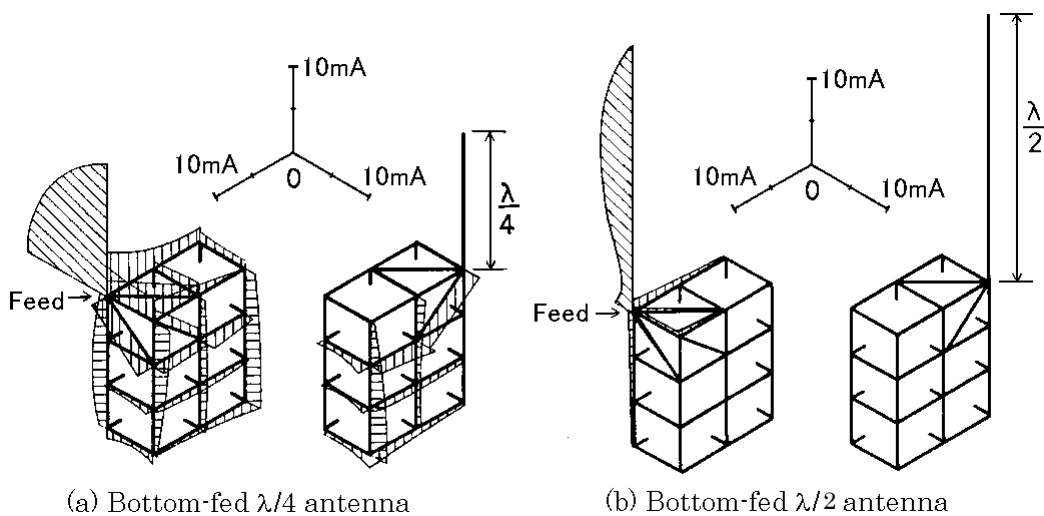
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**Table 1** Overview of antenna for wireless terminal.

	1980-1989	1990-1999		2000-
System	Mobile telephone (800MHz)	PDC (800MHz 1.5GHz)	PHS (1.9GHz)	IMT-2000 (2GHz)
Cavity effect	Half wavelength monopole antenna [1], [2] 3/8 wavelength monopole antenna [1], [2]	Sleeve antenna [17],[18],[19]	Notch on cavity [16]	Half wavelength monopole antenna with feed element [32], [65] Built-in half wavelength dipole antenna [67], [68] Built-in half wavelength monopole antenna [69] Built-in folded dipole antenna [70]
Inverted-F antenna / Small antenna	Planar inverted F antenna (PIFA) [3] Merging with dielectric filter [22] Miniaturization [21] Wideband characteristic [25],[29],[31] User effect reduction [24]	Dual resonance [34]-[37]	Chip antenna [47]-[52] Slot antenna [44],[45]	
Diversity	Antenna coupling effect [5], [60] PIFA for diversity [37]	Arrival wave effect [61] User effect [63] System effect [64]		



**Fig. 1** Current distribution on terminal surface [1], [2].

ence of terminal cavity, evaluated quantitatively radiation patterns of various antennas on terminal cavity by using the moment method and wire grid model [1], [2]. The approximation by wire grid model provides rather high calculation accuracy of radiation pattern, even if the resolution of the model is rather coarse [9].

The results showed that a quarter-wavelength monopole antenna causes rather big leakage current to terminal cavity, in comparison with half-wavelength monopole antenna (Fig.1). Moreover, the results showed that not only the cavity operates as an antenna due to such a leakage current but also length of cavity changes the radiation characteristics of an antenna.

Research on the influence of current on terminal cavity has continued and resulting in the detailed clarification of current distribution on microstrip antenna on a finite ground plane by high-definition grid model [10].

The change of radiation pattern has been investigated by isolating radiations from antenna and terminal cavity individually. The simulation results showed that change of radiation pattern is caused by the difference in phases of these partial radiation patterns [11].

The relation between terminal size and antenna gain has been evaluated by experiments in a real field. The results showed degradation of antenna gain according to terminal size [12].

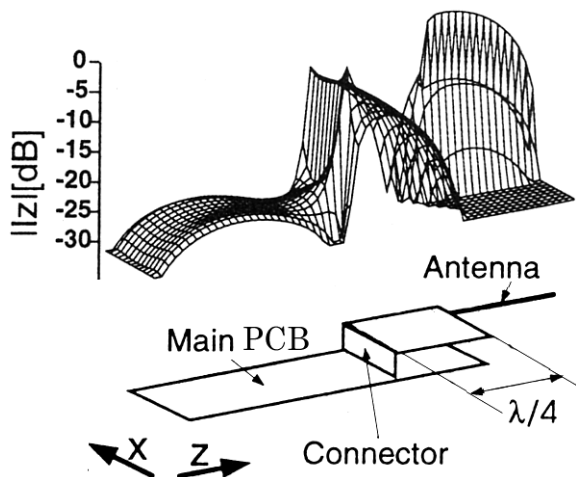


Fig. 2 Current distribution on main printed circuit board [13].

Radiation pattern is also changed by adding planar element to terminal cavity [13]. The planar element is a quarter wavelength and is shorted to terminal cavity; therefore, this element causes a rather strong current distribution on both element and cavity (Fig.2). As this result, these currents cause radiation that cannot be ignored.

### 2.2 Practical Monopole Antennas

Since the input impedance value of a half-wavelength monopole antenna becomes very high, a technical problem arises in that it is hard to match the impedance value with that of a feeding cable. As solutions to this problem, the 3/8 and 5/8 wavelengths monopole antennas have been proposed [1], [2]. These antennas execute greater control of current on terminal cavity than does quarter-wavelength monopole antenna, and provide easier matching with feeding cable than does half-wavelength monopole antenna.

The length of the half-wavelength monopole antenna is also one of the problems. In the case of the PDC terminal operated at 800 MHz, this antenna requires its length of 33cm; that is, this length is not suitable for a handy terminal. Therefore the method for shrinking the antenna length has been proposed [14], [15]. This method employs either a disk or a helical element as a top load element of the monopole antenna, and these elements increase the electrical length of the antenna.

### 2.3 Control of Current on Cavity

A notch on a cavity has been proposed to control current on terminal cavity [16]. A quarter-wavelength notch at the point from a feed point by quarter wavelength realizes change for current on cavity, this notch reduced current on terminal part beyond it (Fig. 3). This method was put into practical use for PHS terminal.

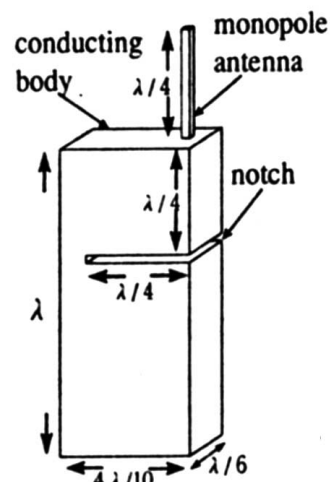


Fig. 3 Monopole antenna on a cavity with notch [16].

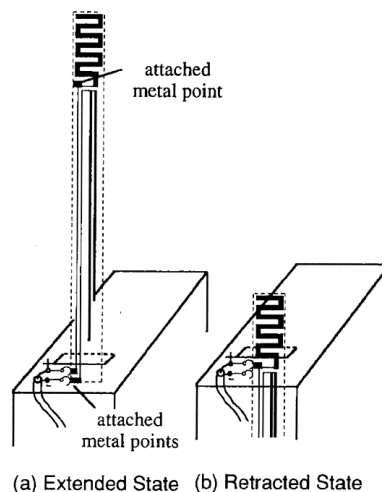
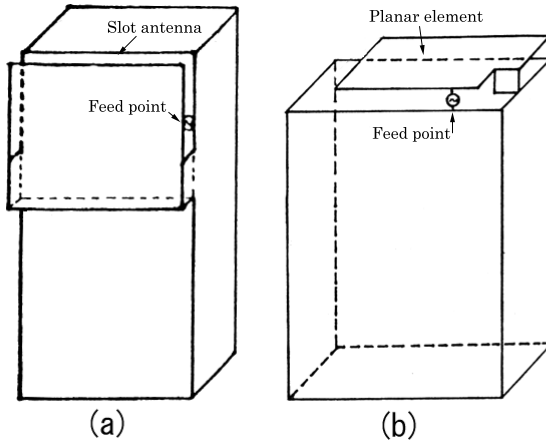


Fig. 4 Retractable sleeve antenna [18].

The characteristics of sleeve antenna with a balun are the same as those of half-wavelength dipole antenna. Also, this antenna reduces current leakage on terminal cavity. The antenna requires flexible feeding cable. Therefore, microstrip line [17] and parallel strip line [18] have been proposed in place of coaxial cable. Furthermore, in order to achieve wideband characteristics of a balun, a method of attaching two baluns has been proposed, and the validity of this antenna was confirmed in [18] and [19](Fig. 4).

### 3. Planar Inverted F Antenna

In order to deal with the expansion of communication area, in 1989 NTT DoCoMo decided to employ a diversity system for cellular phone terminals as a counter measure for fading so as to improve communication performance. To realize the diversity system, planar



**Fig. 5** Cavity slot antenna (a) and planar inverted F antenna (b) for wireless terminal [3], [20].

inverted F antenna was employed.

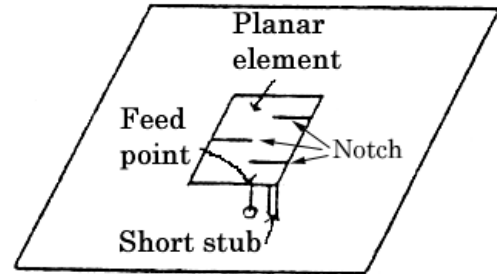
A study on development of built-in antenna was started in 1980, and, as a result, planar inverted F antenna realized [3]. This antenna has a planar element instead of the wire element added on top part of the conventional inverted-F antenna [71]. The antenna was put into practical use for many terminals. This antenna is a current antenna, which is produced by a modification of magnetic-current antenna.

Considering of the validity of magnetic-current antenna in the vicinity of a human body, Haruki et al. started research, which lead to the realization of magnetic-current antenna on cellular phone terminal [20]. Their objective was development of half-wavelength slot antenna, composed of a conductive plate arranged parallel to terminal cavity (Fig. 5(a)). They finally created planar inverted F antenna (Fig. 5(b)). This antenna has a slot, which is composed of a conductive plate whose circumference is half-wavelength and is shorted to terminal cavity at its edge; however, this antenna operates as monopole antenna rather than slot antenna, because current on terminal cavity generates rather strong radiation.

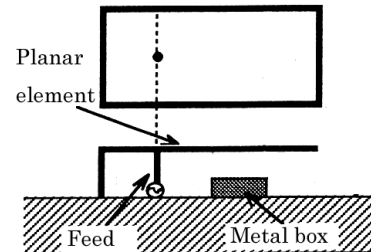
Many researchers have devoted themselves to realizing the practical use of planar inverted F antenna, focusing on miniaturization, achievement of wideband characteristics and development of a new built-in antenna.

### 3.1 Miniaturization Methods

Methods miniaturizing inverted F antenna have been proposed in order to shrink terminal volume. A notch on planar element has been proposed for miniaturization of planar element (Fig. 6). A notch near a feed point was efficient for miniaturization of planar inverted F antenna [21]. This notch operates as a detour for RF current and increases the electrical length of the an-



**Fig. 6** PIFA with notch for miniaturization [21].



**Fig. 7** PIFA with metal box [23].

tenna.

As in the case of microstrip antenna, the method of loading a dielectric between planar element and terminal cavity has been put into practical use for cellular phones [38]. A method of putting a conductive box between planar element and terminal cavity has been proposed [22]. This method was put into practical use by employing a dielectric filter as the box [23] (Fig. 7). Furthermore, a method of bending an edge of a planar element was proposed in [24] (Fig. 12). These methods cause antenna capacitance to increase, which lowers resonance frequency of an antenna.

### 3.2 Methods for Realizing Wideband Characteristics

Three methods have been proposed for realizing the wideband characteristics of inverted F antenna; optimization of the shape of inverted F antenna, addition of an element, and optimization the length of terminal cavity.

It has been clarified that a square is the optimum shape of planar element for realizing wideband characteristics of the antenna [25]. Also, it has been shown that appropriate selection of terminal cavity structure is required for further improvements in antenna bandwidth [6]. Moreover, it has been shown that a half wavelength of terminal cavity achieved maximum bandwidth [26].

With the view to realizing an inverted F antenna with wideband characteristics, a study of a method of adding an element started at an early period. Wideband inverted F antenna, which has an added element near its feed point and also has a parasitic element at

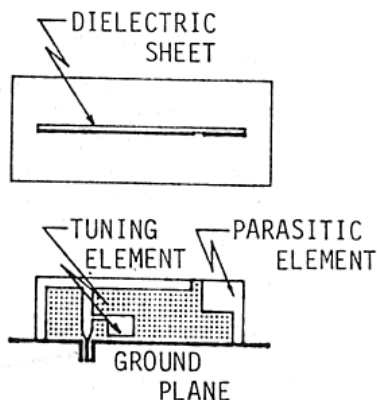


Fig. 8 Print IFA with parasitic element [27].

the open end of antenna element (Fig. 8), has been proposed [27]. The parasitic element causes dual resonance and the added element is for matching its impedance with that of feeding cable.

The antenna, composed of two planar inverted F elements mounted on the same cavity, has wideband characteristics. These characteristics are caused by electromagnetic coupling between two antennas, which differ slightly in size [28].

Also, wideband characteristics have been achieved by adding planar element at a point near the feed point [29]. The parallel resonance characteristics of the additional element cause these wideband characteristics [30]. Wideband characteristics have been achieved by two parallel-fed planar inverted F antennas [31]. This antenna employed two planar inverted F antennas, each having different resonance frequency, and feeding cables whose length was optimized to eliminate antenna coupling (Fig. 9).

A method of adding shorted parasitic element parallel to inverted F antenna has been proposed. The structure of the element, which reverses the feed point and the short point of the antenna, causes strong coupling between antenna and parasitic element [32]. A meander inverted L antenna is proposed as a similar type of this antenna. This antenna realizes a wideband characteristic by using a meander parasitic element, which is fixed under the antenna element [33].

### 3.3 Dual-frequency Operation

To respond to the rapid increase in cellular phone users in the second half of the 90s, NTT DoCoMo had to decide how to expand of its operating frequency band, and several methods were proposed for realizing PIFA for such a requirement.

PIFA with switched short element has been proposed (Fig. 10). The element changes the width of shorted element of PIFA [34]. Shorted microstrip antenna with a slit and loading capacitances on each edge has been proposed [35]. Furthermore, shorted mi-

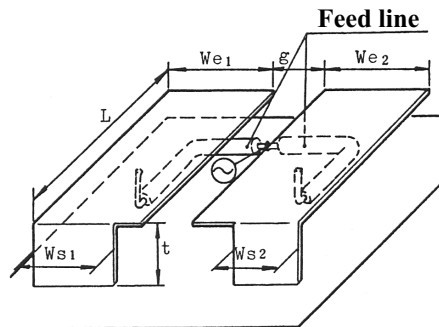


Fig. 9 PIFAs fed by parallel lines [31].

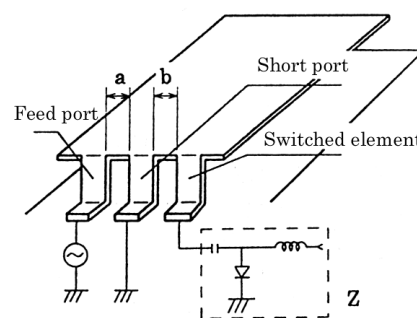


Fig. 10 PIFAs with switch element[34].

crostrip antenna with a slot on its planar element has been proposed. This slot operates as both a round-about path for a low-frequency current and a choker for a high-frequency current [36].

### 3.4 Reduction of Influence from Human Body

The first influence from the human body to be noted was a change of terminal angle in the talk position. According to measured statistical data, the inclined angle was almost 60 degrees. The influence of a mounted position of planar inverted F antenna on terminal cavity was investigated in the case of such an angle, and the result showed that type C in Fig. 11 realized high averaged gain [37].

Directivity characteristics of inverted F antenna are employed to reduce an influence from a human body [24]. Inverted F antenna mounted on the center area of terminal cavity has good F/B ratio. Because of such these characteristics, an influence from the human body behind an antenna is reduced (Fig. 12). In order to investigate these characteristics in detail, the F/B ratios of planar inverted F antenna mounted on terminals of various lengths have been clarified [38].

Furthermore, it has been clarified that an operation frequency changed degradation of radiation efficiency of planar inverted F antenna by a human body [39]. This study progressed and it has been clarified that shorted microstrip antenna had an efficient per-

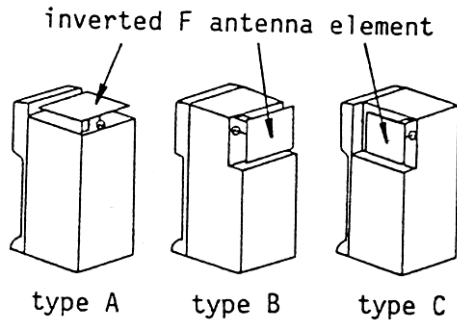


Fig. 11 Mounted side of planar inverted F antenna [37].

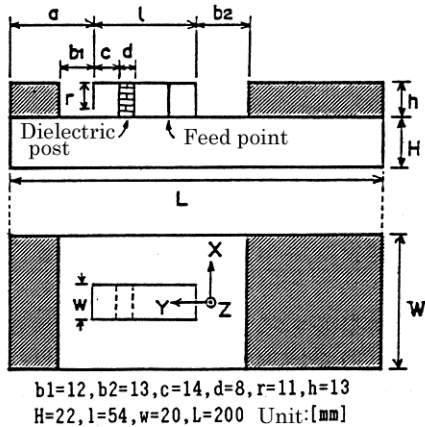


Fig. 12 inverted F antenna for reducing influence from a user [24].

formance because of its rather high directivity [40].

### 3.5 Other Built-in Type Antennas

Besides the inverted F antenna, various low-profile monopole antennas have been proposed. They include folded monopole antenna (Fig. 13) [41], S-shaped antenna (Fig. 14)[42], and shorted microstrip antenna fed by electrical coupling element [43].

The last-named antenna achieved dual-frequency operation by using switched element coupled with planar element.

Cavity back slot antenna for wireless terminal has been realized and put into practical use on a PHS terminal [44]. Based on this antenna, tunable resonance antenna was realized by putting switched element in its slot [45] (Fig. 15).

One of the problems concerning terminal antennas is that the posture of a terminal often changes. Rotating microstrip antenna was proposed as a solution to this problem. This antenna is fed by an electromagnetically coupled feeder, which also acts as an axis of rotational element [46].

A dielectric loaded antenna is known as a small volume antenna [2]. This antenna has progressed uniquely in Japan; that is, the antenna has become a low profile.

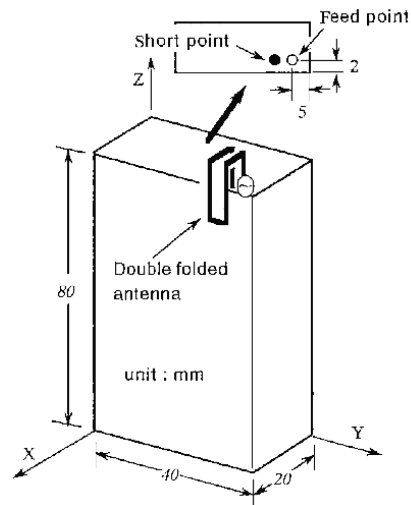


Fig. 13 Folded monopole antenna [41].

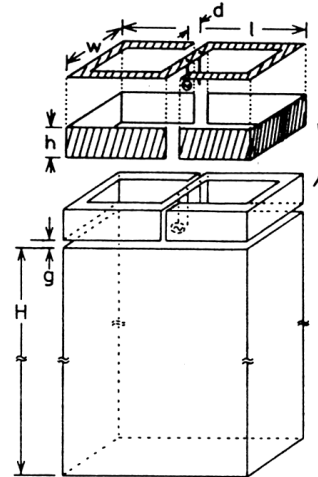


Fig. 14 S-type antenna [42].

This progress realizes a surface mount like other chip parts by a chip-mounting machine.

This antenna includes a monopole antenna type [47],[49] and an electrical coupled antenna type [47]-[52] (Fig. 16). Monopole antenna type realizes a drastic miniaturization by employing a helical element [49], and electrical coupled antenna type has a wideband characteristic [47]-[50]. Both of two types are put in practical use; and, recently, an influence from a human body is studied [51],[52].

Moreover the antenna technologies for pagers are briefly reviewed here.

Fujimoto et al. reported the first important results. They clarified that magnetic-current antenna is suitable for use in the vicinity of a human body [2]. For example, gain of loop antenna is raised when it is arranged perpendicular to the human body, because its aperture is almost doubled by the human body,

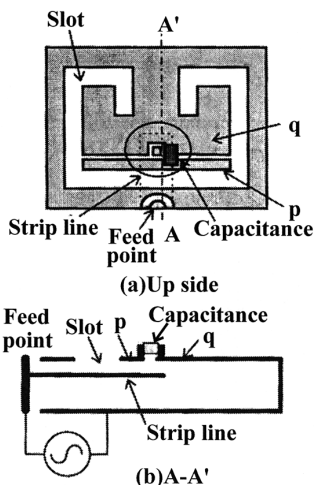


Fig. 15 Slot antenna with variable capacitance [45].

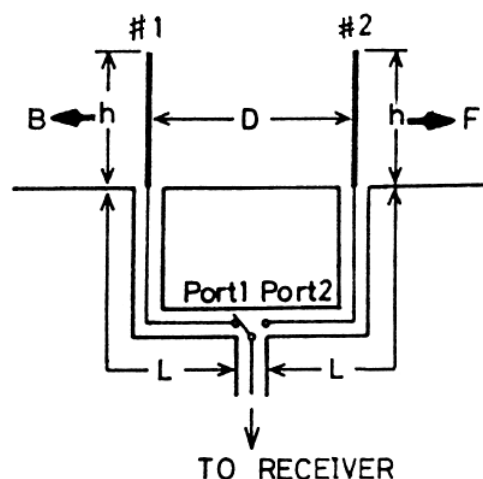


Fig. 17 Monopole antennas for antenna selection diversity [5].

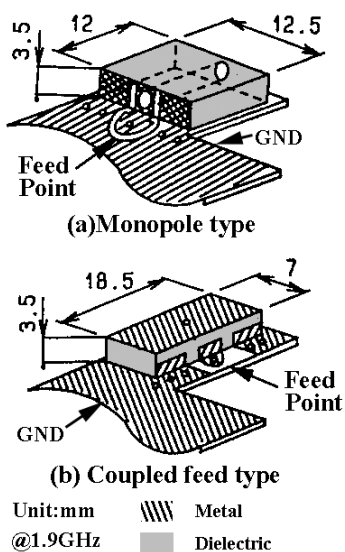


Fig. 16 Two types of chip antenna [47].

which works as a ground plane. This research resulted in miniaturization and low-profile pager antenna [53], and it resulted in the development of an antenna for a wristwatch-type terminal [54].

#### 4. Diversity System

In line with the expansion of a communication area, a counter measure for fading has been required order to improve communication performance. Therefore, NTT DoCoMo decided to employ a diversity system for cellular phone terminals. This decision opened up new technical subjects, for example, design methods for diversity antennas mounted on terminal cavities.

#### 4.1 Diversity Antenna with Electromagnetic Coupling

Sawaya et al. proposed optimization of correlation coefficient between monopole antennas on a ground plane (Fig. 17) by using electromagnetic coupling between antennas [5]. A feed line for an unselected branch works as reactance element for antenna selection diversity. The reactance values change the strength of electromagnetic coupling between antennas. The coupling changes a radiation pattern of antennas; and the radiation pattern changes correlation coefficient between antennas. Therefore, correlation coefficient keeps a small value by optimization of the length of feed lines.

Recently, this method has been employed for diversity antennas for terminals [55]. Using a terminal model consisting of a combination of monopole antenna and inverted F antenna, it was found that electromagnetic coupling lowers correlation coefficient but then degrades matching characteristics. Therefore, an optimization method for the shape of an inverted F antenna has been proposed in place of electromagnetic coupling to lower correlation coefficient. Moreover, a design method for termination reactance of inverted F antenna has been proposed as a method of reducing electromagnetic coupling [56].

#### 4.2 Evaluation of Diversity Performance

In the early stage of the study on diversity antennas for cellular phone terminals, correlation coefficient was clarified only as an experimental result.

Taga and Tsunekawa clarified correlation coefficient of two planar inverted F antennas mounted on terminal cavity in outdoor experiments (Fig. 18) [57], [58]. The moment method with wire grid model has been employed to simulate diversity antennas; characteristics of two dipole antennas arranged on top of terminal cavity have been calculated. The results showed

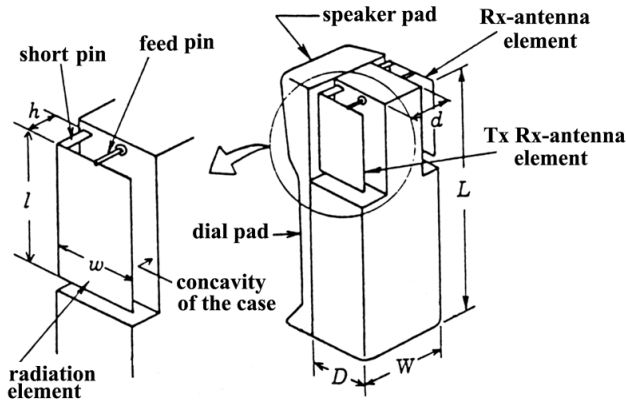


Fig. 18 PIFA for diversity antenna [57].

that a value of correlation coefficient is relatively low when the distance between the antennas is comparatively small, because radiation patterns are changed by electromagnetic coupling between antennas [59], [60].

In order to count on a distribution of an arrival wave to an evaluation of an antenna for a cellular phone, the distribution over solid angles in a real field of an urban area has been measured, and a typical value was obtained [61]. Furthermore, performance of polarization diversity antenna, which is constructed by a cross dipole antenna, was evaluated by using the typical distribution values, and the obtained results showed the validity of the typical value.

Correlation coefficient between half-wavelength monopole antenna and planar inverted F antenna mounted on a terminal has been evaluated under various arrival wave distributions [63],[62].

In order to predict diversity gain of a real terminal, it is necessary to consider the details of a radio system. Diversity gain of an antenna mounted on a terminal has been evaluated in the case of the PDC communication system [64].

## 5. The Latest Topics; Antennas after IMT2000 Terminals in Japan

In 2001, the IMT2000 system service started in Japan. The terminals for W-CDMA system employed built-in antenna or half-wavelength monopole antenna. This section reviews these antenna technologies.

### 5.1 Half-Wavelength Monopole Antennas

2GHz band is employed for the IMT2000 system, because its rather short wavelength provides flexibility in antenna design; for example, half-wavelength monopole antenna is employed.

Half-wavelength monopole antenna requires a matching circuit; therefore quarter-wavelength element is employed for a matching circuit. Electromagnetic coupling of these two elements has been proposed

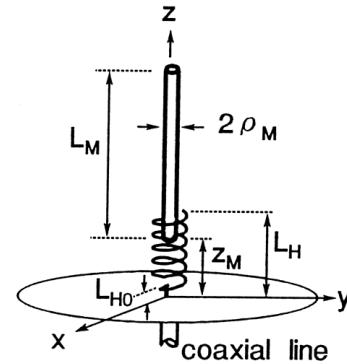


Fig. 19 Half-wavelength monopole antenna fed by helical element [32].

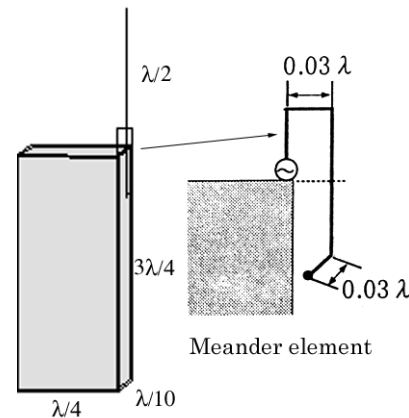


Fig. 20 Half-wavelength monopole antenna fed by meander element [65].

for realizing both wideband characteristics and dual-frequency operation [32] (Fig. 19).

Undesired radiation from quarter-wavelength element is one of an important issue. It has been clarified that fixing a connecting point of these two elements close to the surface of a terminal cavity reduced surface current [65] (Fig. 20).

### 5.2 Built-in Half-Wavelength Antenna

In 1986, Taga and Tsunekawa proposed a built-in dipole antenna with a balun in their patent [66]. The antenna has been restored for the IMT2000 terminal (Fig. 21) [67]. They proposed a wideband method for the antenna in which parasitic element is used.

A method of arranging a built-in dipole antenna into a flip portion of a terminal has been proposed (Fig. 22). This antenna employs a matching circuit, which changes an antenna impedance in accordance with the opening-and-closing state of a flip [68].

T-type monopole antenna that operates in a parallel resonance mode has been proposed. This antenna is a microstrip dipole antenna, and its self-resonance characteristic avoids undesired radiation from terminal



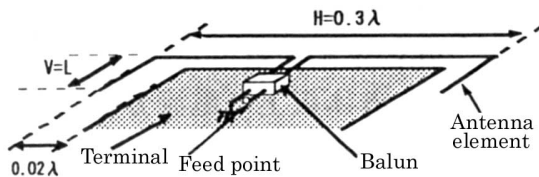


Fig. 21 built in type dipole antenna [67].

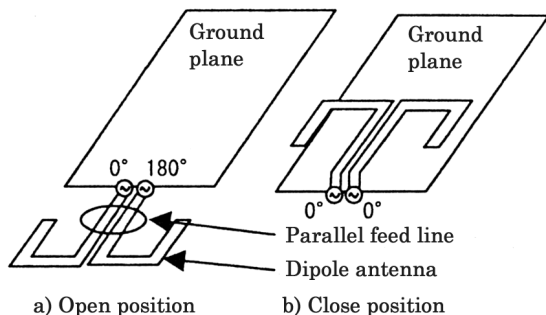


Fig. 22 built in type dipole antenna on terminal flip [68].

cavity. [69].

Morishita et al. has proposed a folded dipole antenna [70]. A novel folded loop antenna (Fig. 23) for a wireless terminal has been proposed together with an advanced design concept [70] for handset antennas.

The design concept satisfies the principal requirement for terminal antennas namely (1) small size and yet (2) has capability of mitigating degradation of antenna performance due to the body effect, and (3) of reducing SAR value in the human head at the handset talk position, in addition to the indispensable requirements for handset antennas such as (4) low profile, and (5) light weight.

The technology makes this antenna (a) an integrated structure, which is a typical application of a fundamental concept for making antennas small and (b) a balanced structure which has been proved to be very effective in satisfying requirements (2) and (3).

The folded loop antenna is essentially a two-wire transmission line, folded at about a quarter-wavelength to form a half-wave folded dipole, and yet appears to be a loop of one wavelength. This antenna also has an integrated structure, which is composed of radiation element and reactive element; these being constituted by using a two-wire transmission line, and folded at a quarter-wavelength to form a folded half-wave dipole equivalently. The equivalent folded dipole acts mainly as the radiator and the two-wire line is used for adjusting the antenna impedance [72]. This antenna can be designed to have enough gain and bandwidth to be applied to handsets currently in practical use.

### 6. Conclusion

This paper has reviewed technologies for terminal cav-

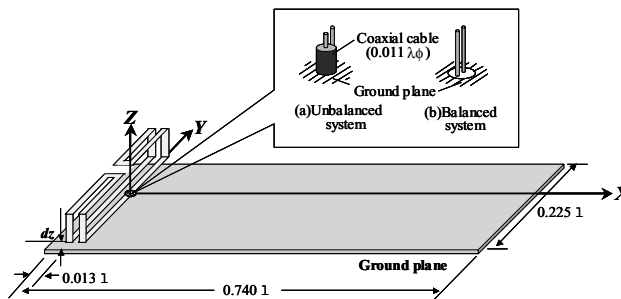


Fig. 23 Built-in folded dipole antenna [70].

ity current, small antennas and diversity antenna. Antenna technology for cellular phones has long been extensively researched in Japan. This research has contributed to the miniaturization of terminals used worldwide. The technology developed as a result of this research is expected to be applied in development of smart antennas (beam scan, wideband characteristic) for IMT2000 terminals from now on.

### References

- [1] K. Hirasawa and K. Fujimoto, "Characteristic of Wire Antennas on a Rectangular Conducting Body," *Trans. IEICE Japan*, J65-B-9, pp.1133-1139, 1982
- [2] K. Fujimoto, A. Henderson, K. Hirasawa, and J.R. James, *Small antenna, Research Studies Press* 1987
- [3] H. Haruki and T. Kobayashi, "Inverted F antenna for UHF Portable Equipment," 1982 National Convention Record of IEICE Japan, 3-66, pp.613, 1982 (in Japanese)
- [4] K. Sato, K. Matsumoto, K. Fujimoto and K. Hirasawa, "Characteristic of a planar Inverted-F antenna on a rectangular conducting body." *Trans. IEICE B-II*, vol.J71-B no.11, pp.1237-1243, Nov. 1988. (in Japanese)
- [5] K. Sawaya, T. Ishizone, and Y. Mushiake, "A correlation coefficient between two monopole antennas for an antenna selection diversity system," 1982 National Convention Record of IEICE Japan, 3-63, pp.610, 1982 (in Japanese)
- [6] T. Taga and K. Tsunekawa, "Performance Analysis of a Built-in Planar Inverted F Antenna for 800 MHz Band Portable Radio Units," *IEEE J. Sel. Areas Commun.*, SAC-5-5, 921, 1987
- [7] K. Fujimoto, "Overview of antenna systems for mobile communications and prospects for the future technology," *IEICE Trans. vol.E 74*, no.10, Oct. 1991
- [8] S. Tokumaru, "Electrically small antennas," *Trans. IEICE Japan*, J71-B, no.11, pp.1206-1112, 1988 (in Japanese)
- [9] T. Uno, "Handset antennas," *Proc. 1997 IEICE general conf.*, IEICE Japan, TB-1-4, pp.751, 1997 (in Japanese)
- [10] H. Morishita, K. Fujimoto and K. Hirasawa, "Analysis of rectangular microstrip antenna having the same width as the ground plane," *Trans. IEICE Japan*, vol.J71-B no.11, pp.1274-1280, 1988
- [11] R. Yamaguchi, K. Sawaya, Y. Fujino, and S. Adachi, "Effect of dimension of conducting box on radiation pattern of a monopole antenna for portable telephone" *IEICE Trans. Commun. vol.E76-B*, no.12, pp.1526-1531, Dec. 1993
- [12] H. Arai, N. Igi, H. Hanaoka, "Antenna-Gain Measurement of Handheld terminals at 900MHz," *IEEE Trans. on vehicular technology*, vol.46, no.3, Aug. 1997
- [13] A. Tsujimura, S. Sekine, H. Shoki and Y. Suzuki, "A study

- of the current distribution on the dual printed circuit boards for a portable radio phone" Proc. 1998 IEICE general conf. B-1-116, pp.116, 1998 (in Japanese)
- [14] K. Ogawa and T. Uwano, "Analysis of a diversity antenna comprising a whip antenna and a planar inverted F antenna for portable telephone (IN Japanese)," IEICE Trans. B-II vol.J79-B-II, no.12, pp.1003-1012, Dec. 1996
  - [15] N. Koike, "Antenna and wireless terminal," Japanese patent P2501413, USP5434582
  - [16] S. Sekine and T. Maeda, "The radiation characteristic of a 1/4 monopole antenna mounted on a conducting body with a notch," IEEE AP-S 1992 Digest 1, pp.65-68, 1992
  - [17] Y. Yoshikawa, Y. Sunahara and M. Matsunaga, "Coil loaded sleeve antenna fed by microstrip line," Proc. 1991 IEICE Fall conf., IEICE Japan, B-104, vol.2, pp.104, 1990 (in Japanese)
  - [18] K. Tsunekawa, "High performance portable telephone antenna employing a flat-type open sleeve," IEICE Trans. Electron. vol.E79-C, no.5, pp.693-698, May 1996
  - [19] Y. Nishioka, T. Fukasawa and H. Omine, "Dual-band planar sleeve antenna for portable wireless terminal," Proc. 2001 IEICE general conf., IEICE Japan, B-1-122, pp.122, 2001 (in Japanese)
  - [20] H. Haruki, Y. Hiroi, T. Taga and H. Mishima, "Slot antenna for UHF Portable Equipment," National Convention Records on opt and electrical wave, IEICE Japan, 40, pp.40, 1980 (in Japanese)
  - [21] K. Tsunekawa and T. Taga, "A Study of Miniaturized Inverted-F Type Antennas" 1984 National Convention Record 3-19, pp.624, 1984(in Japanese)1984
  - [22] S. Sato, T. Ebisui, Y. Sunahara and F. Takeda, "Input Impedance Characteristics of Planar Inverted F Type Antenna Having a Capacitance," 1985 National Convention Record, IEICE Japan, S5-2, vol.3 pp.249, 1985 (in Japanese)
  - [23] T. Endo and S. Sato, "Equivalent capacitance of short patch antenna with conducting block," Proc. 1996 IEICE general conf., IEICE Japan, B-65, pp.65, 1996 (in Japanese)
  - [24] Y. Oshima and N. Goto, "Radiation Pattern of Small Antennas for Mobile Communications," 1986 National Convention Record, IEICE Japan, 636, vol.3 pp.73, 1986 (in Japanese)
  - [25] K. Tsunekawa, "Bandwidth Characteristics of Planar Inverted F antenna," 1988 National Convention Record, IEICE Japan, B-65, vol.1 pp.65, 1988 (in Japanese)
  - [26] K. Tsunekawa, "Band width of a planar inverted F antenna on a small metal housing," Proc. 1996 Commn. Society Conf. IEICE, IEICE Japan, B-84, pp.84, 1996 (in Japanese)
  - [27] H. Mishima and T. Taga, "Mobile Antennas and Duplexer for 800MHz Band Mobile Telephone System," IEEE AP-S proceedings AP.14-5 pp.508-511, 1980
  - [28] T. Komori, "Diversity antenna for a cellular phone," Technical report of Mushiake lab. Tohoku University, 1984 (in Japanese)
  - [29] T. Ishizone, S. Sekine, H. Ishikawa and S. Nishida, "Impedance Characteristics of Inverted-F Antenna with Matching Plate," 1986 National Convention Record, IEICE Japan, 675,vol.3, pp.112, 1986 (in Japanese)
  - [30] S. Sekine, T. Ito, Y. Murakami, and H. Shoki, "Broadband characteristic of inverted-F antenna by parallel resonance mode," Proceedings of the 02-i ISAP (Japan),pp.243-246, Nov. 2002
  - [31] Y. Yokoyama and N Goto, "Dual-Resonance Broad Band Microstrip Antenna," Proceedings of ISAP '85, 121-2, pp.429-432, 1985
  - [32] H. Nakano, N. Ikeda, Y. Wu, R. Suzuki, H. Mimaki and J. Yamauchi, "Realization of dual-frequency and wide-band VSWR performance using normal-mode helical and inverted-F antennas," IEEE Trans. Antennas Propagat., vol.46, no.6, pp.788-793, June 1998
  - [33] K. Noguchi, N. Yasui, M. Mizusawa, and S. Betsudan, "Impedance Characteristic of a Meander-Line Antenna Mounted On a Conducting Plane," Proc. 1999 IEICE general conf., IEICE Japan, B-1-106, pp.106, 1999 (in Japanese)
  - [34] T. Saito, S. Nakamura, N. Kohyama and Y. Yokoyama, "A dual band inverted F antenna with a switched device," Proc. 1997 IEICE general conf., IEICE Japan, B-1-74, pp.74, 1997 (in Japanese)
  - [35] S. Hagiwara and K. Tsunekawa, "Small directional antenna with dual resonant characteristic for a portable radio unit," Proc. 1997 IEICE general conf., IEICE Japan, B-1-75, pp.75, 1997 (in Japanese)
  - [36] T. Amano, N. Chiba and Iwasaki, "A Quarter-Wavelength Shorted Microstrip Antenna with a Slot for Dual-Frequency Operation," IEICE trans. electron., vol.E82-C, no.7, pp.1211-1216, July 1999
  - [37] T. Taga and K. Tsunekawa, "A built-in diversity antenna for 800 MHz band portable radio units," Proceedings of ISAP '85, 121-1, pp.425-428, 1985
  - [38] M. Kaneoya, M. Hirose and T. Sekido, "Radiation pattern of inverted-F antenna for PHP," Proc. 1993 IEICE fall conf., IEICE Japan, B-117, vol.2, pp.117, 1993 (in Japanese)
  - [39] K. Sato, K. Nishikawa and N. Suzuki, "Analysis of antenna mounted on portable equipment near human body," Proc. 1996 IEICE general conf., IEICE Japan, B-161, pp.161, 1996 (in Japanese)
  - [40] S. Hagiwara and K. Tsunekawa, "Analysis of housing current properties by planar antenna attached on a small metal housing," Proc. 1995 Commn. Society conf. IEICE, IEICE Japan, B-113, pp.113, 1995 (in Japanese)
  - [41] Y. Kumon and T. Tsukiji, "Characteristic of a double folded monopole antenna for the mobile telephone," Trans. IEICE Japan, J81-B-II, no.11, pp.1073-1076, 1998
  - [42] K. Suda, K. Sawaya, K. Igari and S. Adachi, "Built-in S-shaped antenna for portable telephone," Trans. IEICE Japan, J71-B, no.11 pp.1365-1367, 1988
  - [43] H. Takebe and K. Higashi, "Mobile phone antenna with a switch for dual band use," Proc. 1997 Commn. Society conf. IEICE, IEICE Japan, B-1-52, pp.52, 1997 (in Japanese)
  - [44] K. Takei, H. Okabe and Y. Imakado, "A planar slot antenna for portable radio phone terminal," Proc. 1997 IEICE general conf, IEICE Japan, B-1-69, pp.69, 1997 (in Japanese)
  - [45] H. Okabe, K. Takei, and K. Higuchi, "A tunable planar slot antenna for portable radio phone terminal," Proc. 1997 Commn. Society conf. IEICE, IEICE Japan, B-1-50, pp.50, 1997 (in Japanese)
  - [46] A. Ando, Y. Honma and K. Kagoshima, "A novel electromagnetically coupled microstrip antenna with a rotatable patch for personal handy-phone system units," IEEE Trans. Antennas Propag. vol.46, no.6, pp.794-797, June 1998
  - [47] K. Kawahata, K. Yamaki, Y. Saitoh and S. Arai, "SMD antenna for portable telephone," Proc. 1994 IEICE spring conf., IEICE Japan, B-129, pp.129, 1994 (in Japanese)
  - [48] H. Matsushima, E. Hirose, Y. Shinohara, H. Arai and N. Goto, "Electromagnetically coupled dielectric chip antenna," Proc. 1998 IEICE general conf., IEICE Japan, B-1-112, pp.112, 1998 (in Japanese)
  - [49] K. Watanabe, S. Kanba, T. Tsuru and H. Mandai, "Wide Band Type Chip Multilayer Antenna," Proc. 1998 Commn. Society conf. IEICE, IEICE Japan, B-1-44, pp.44, 1998 (in Japanese)
  - [50] Y. Dakeya, S. Kanba, T. Tsuru and H. Mandai, "GND Type Chip Multilayer Antenna," Proc. 1998 Commn. So-

- ciety conf. IEICE, IEICE Japan, B-1-45, pp.45, 1998 (in Japanese)
- [51] A. Miyata, K. Kawahata, Y. Saitoh and Y. Ishikawa, "Evaluation of chip dielectric antennas mounted on ground plane close to dry phantom," Proc. 1999 IEICE general conf., IEICE Japan, SB-1-10, pp.650, 1999 (in Japanese)
- [52] H. Arai and S. Sakai, "A Design of uni-directional portable terminal antenna and effect of phantom," Proc. 1999 IEICE general conf., IEICE Japan, SB-1-12, pp.652, 1999 (in Japanese)
- [53] N. Ishii and K. Itoh, "A Consideration of the Thin Planar Antenna with Wire-Grid Model," IEICE Trans. Communications, E76-B, 12, pp.1518-1525, Dec. 1993
- [54] Y. Okano and K. Ito, "A study on small slot antenna for wristwatch type portable radio equipment," Proceedings of TJSAP'97, pp.173-176, May 1997.
- [55] S. Sekine, N. Odachi, O. Shibata, H. Shoki and Y. Suzuki, "Novel design method for antennas for selection diversity on wireless terminal," IEICE Trans. Commun., VOL. E84-B, NO.9, pp.2451-2459, Sept. 2001
- [56] N. Odachi, S. Sekine, H. Shoki and Y. Suzuki, "A Novel Analytical Method for Optimizing the Terminating Impedance of an Inverted-F Antenna for Antenna Selection Diversity on a Hand-Held Phone," IEICE Trans. Commun., vol.E84-B no.1 pp.89-94, Jan. 2001
- [57] T. Taga and K. Tsunekawa, "A built-in diversity antenna for 800 MHz band portable radio units," IEEE AP-S 1986 Digest 2 vol.vi+1044, pp.705-708, 1986
- [58] K. Tsunekawa, "Diversity antennas for portable telephones," 39th IEEE VTC 2 vol.901, vol.1, pp.50-56, 1989
- [59] K. Tsunekawa and K. Kagoshima, "Correlation coefficients of diversity antennas on a small metal body," Proceedings of the 1989 ISAP (Japan) 4, vol.3, pp.585-588, 1989
- [60] K. Tsunekawa and K. Kagoshima, "Diversity performance analysis of two parallel dipole antennas mounted on a small metal body," Electron. Commun. Jpn. 1, Commun. vol.76, no.10, pp.80-90, Oct. 1993
- [61] T. Taga, "Analysis for correlation characteristics of antenna diversity in land mobile radio environments (IN Japanese)," Trans. IEICE B-II vol.J73B-II, no.12, pp.883-895, Dec. 1990
- [62] K. Ogawa, T. Uwano, M. Kanda, and Y. Morinaga, "Diversity antenna for 800 MHz-band digital cellular mobile telephones (IN Japanese)," Natl. Tech. Rep. vol.42, no.1, pp.143-148, Feb. 1996
- [63] K. Ogawa and T. Uwano, "A diversity antenna for very small 800-MHz band portable telephones," IEEE Trans. Antennas Propagat. vol.AP-42, no.9, pp.1342-1345, Sept. 1994
- [64] K. Ogawa and J. Takada, "An analysis of the effective performance of a handset diversity antenna influenced by head, hand and shoulder effects - A proposal for the diversity antenna gain based on a signal bit-error rate and the analytical results for the PDC system," IEICE Trans., vol.J83-B, no.6, pp.852-865, June 2000.
- [65] N. Odachi, S. Sekine, H. Shoki and Y. Suzuki, "A rod antenna with a meander element for handheld phone terminal," Proc. 1999 Comm. Society conf. IEICE, IEICE Japan, B-59, pp.59, 1999 (in Japanese)
- [66] T. Taga, I. Takekawa and K. Tsunekawa, "Wireless terminal," Japanese patent, Toku-Kai-Syo 61-205004
- [67] K. Egawa, T. Oga and H. Itoh, "Radiation characteristic of U-dipole antenna for cellular phone," Proc. 2000 IEICE general conf., IEICE Japan, B-1-123, pp.123, 2000 (in Japanese)
- [68] T. Fukasawa, Y. Nishioka, H. Ohmine and S. Urasaki, "Characteristics of dipole antenna built in flip of dipole

telephone ", Trans. IEICE vol.J85-B no.6, pp.941-952, June 2002 (in Japanese)

- [69] S. Sekine and H. Shoki, "Wideband characteristics of T type monopole antenna on parallel resonance mode," Proc. 2000 Comm. Society conf. IEICE, IEICE Japan, B-1-120, pp.120, 2000 (in Japanese)
- [70] Y. Kim, H. Morishita, Y. Koyanagi and K. Fujimoto, "A folded loop antenna system for handsets design developed and based on the advanced design concept," IEICE Trans. Commun., vol.E84-B, no.9, pp.2468-2475, Sept. 2001
- [71] K. Nagai and T. Sato, "Radiation characteristic of shunt driven inverted L antenna," National Convention Record of 50th anniversary of IECE, IECE Japan, 395, pp.395, 1977 (in Japanese)
- [72] H. Uchida and Y. Mushiake, VHF-Antenna, Corona Publishing CO., LTD., Japan, 1955.



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